

TITLE OF THE INVENTION

Assembling Method of Tire and Wheel Rim

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to an assembling method of a tire and a wheel rim, which can lighten a gravity of a balance weight for correcting a weight unbalance in an assembled structure of the tire and the wheel rim.

Description of the Related Art

When a weight unbalance exists in an assembled structure of a tire and a wheel rim, a vehicle vibration is caused. Therefore, in order to reduce the weight unbalance mentioned above, it has been conventionally, generally carried out to assemble the tire in the wheel rim in a state of aligning a phase of an air valve position regarded as a heavy point of the wheel rim with a phase of a light point of the tire. Thus, it is possible to cancel a part of the weight unbalance, so that it is possible to reduce the gravity of the balance weight for correcting the weight unbalance in the assembled structure of the tire and the wheel rim.

However, the balance weight mentioned above is normally mounted to the leading end of the rim, thereby deteriorating an outer appearance and causing a cost increase. Therefore, it is desired to further reduce the weight.

In view of such a circumstance, the present inventor has studied. As a result, the present inventor has found that the effect of canceling the

weight unbalance can be enhanced and the gravity of the balance weight can be more reduced, by assembling the tire and the wheel rim while taking into consideration a Radial Runout (RRO) corresponding to an eccentricity of the wheel rim.

More specifically, the wheel rim 1 generally has an average RRO of the order of 0.4 mm and, as conceptually shown in Fig. 5A, a center displacement δ is generated between a center of rotation i and a center j of an outer periphery of a rim sheet 1a. On the other hand, the tire 10 is approximately concentrically attached to the rim sheet 1a. Therefore, a moment corresponding to a product $T_t \times \delta$ of a tire weight T_t and the displacement δ is applied around the rotation center i, and a further weight unbalance is generated.

Accordingly, it has been found that the effect of canceling the weight unbalance can be more enhanced, and the gravity of the balance weight can be further reduced, on the basis of the following matters (1) and (2), as conceptually shown in Fig. 5B.

(1) A vector \overrightarrow{Wc} of a correction unbalance is determined by adding a vector \overrightarrow{Wub} of a weight unbalance of a wheel rim itself to a vector $\overrightarrow{W1}$ of a weight unbalance based on the RRO.

(2) The tire and the wheel are assembled by aligning a phase of the vector \overrightarrow{Wc} with the phase of the light point of the tire.

SUMMARY OF THE INVENTION

An object of the present invention is to provide a method of assembling a tire and a wheel rim which can increase an effect of canceling a

weight unbalance to the maximum, and can further reduce a gravity of the balance weight.

In order to achieve the object mentioned above, in accordance with a first aspect of the present invention, there is provided a method of assembling a tire and a wheel rim, comprising the steps of:

(1) determining a Radial Runout (RRO) value $Wr1$ (unit: mm) in a primary component of the RRO of the wheel rim, a phase $\theta r1$ (unit: °) of a peak position thereof, an unbalance level Wub (unit: g) of a heavy point in a weight unbalance of the wheel rim, a phase θub thereof (unit: °), a radial distance L (unit: mm) of a balance weight mounting position for correcting the weight unbalance from an axis center of the wheel rim, a weight Tt (unit: mm) of the tire, and a phase αt of a light point in the weight unbalance of the tire;

(2) determining a phase θc of a correction unbalance Wc found by the following formula (1), by using the RRO value $Wr1$, the phase $\theta r1$, the unbalance level Wub , the phase θub , the distance L , the weight Tt and the phase αt determined in the preceding step; and

$$\theta c = \tan^{-1} \left[\frac{Wub \times \sin \theta ub + \{ (Wr1 \times Tt) / (2 \times L) \} \times \sin \theta r1}{Wub \times \cos \theta ub + \{ (Wr1 \times Tt) / (2 \times L) \} \times \cos \theta r1} \right] \dots (1)$$

(3) assembling the tire and the wheel rim in a state of aligning the phase θc of the correction unbalance Wc with the phase αt of the light point of the tire.

BRIEF DESCRIPTION OF THE DRAWINGS

Fig. 1 is a flow chart describing a method of assembling a tire and a

wheel rim in accordance with the present invention;

Fig. 2 is a diagram describing the assembling method;

Fig. 3 is a graph showing an average curve determined by a RRO curve of rim sheets in both sides;

Fig. 4 is a wave form chart of a primary component determined by an order analysis of the average curve;

Fig. 5A is a diagram describing an influence applied to a weight unbalance by the RRO, and Fig. 5B is a vector diagram describing a correction of a weight unbalance of the wheel rim by the RRO; and

Figs. 6A and 6B are diagrams each showing a relation between a weight unbalance level of the tire in Table 2 and an effect of reducing the gravity of the balance weight.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Hereinafter, description will be given of an embodiment in accordance with the present invention with reference to the accompanying drawings. Fig. 1 is a flow chart describing a method of assembling a tire and a wheel rim (hereinafter, referred to as an assembling method) in accordance with the present invention, and Fig. 2 is a diagram describing the assembling method.

In Figs. 1 and 2, the assembling method comprises the following steps:

(1) step S1 of determining a Radial Runout (RRO) value $Wr1$ (unit: mm) in a primary component of the RRO of a wheel rim 1, a phase $\theta r1$ (unit: °) of a peak position thereof, an unbalance level Wub (unit: g) of a heavy point

in a weight unbalance of the wheel rim 1, a phase θ_{ub} thereof (unit: °), a radial distance L (unit: mm) of a balance weight mounting position J for correcting the weight unbalance from an axis center i of the wheel rim, a weight T_t (unit: mm) of a tire 10, and a phase α_t of a light point in the weight unbalance of the tire 10;

(2) step S2 of determining a phase θ_c of a correction unbalance W_c found by the following formula (1), by using each of the values determined in step S1; and

$$\theta_c = \tan^{-1} \left[\frac{[W_{ub} \times \sin \theta_{ub} + \{(W_{r1} \times T_t)/(2 \times L)\} \times \sin \theta_{r1}]}{[W_{ub} \times \cos \theta_{ub} + \{(W_{r1} \times T_t)/(2 \times L)\} \times \cos \theta_{r1}]} \right] \dots (1)$$

(3) step S3 of assembling the tire and the wheel rim in a state of aligning the phase θ_c of the correction unbalance W_c with the phase α_t of the light point of the tire 10.

In step S1, the primary component of the RRO of the wheel rim 1 is determined by measuring the RRO of the rim sheets 1a in both sides of the wheel rim 1 and order analyzing an average curve Y of the RRO curves Y_1 and Y_2 as shown in Figs. 3 and 4.

More specifically, the RRO of each of the rim sheets 1a can be easily measured by using a well-known measuring device such as a contact type displacement gauge. Further, the average curve Y can be obtained by overlapping and averaging the RRO curves Y_1 and Y_2 of the respective rim sheets 1a from the measurement result with each other, and a wave form of the primary component (a primary wave form) of the RRO is introduced by order analyzing the average curve Y , as shown in Fig. 4. Thus, the RRO value W_{r1} in the primary wave form and the phase θ_{r1} of the peak position P

corresponding to the maximum crest portion of the primary wave form are determined. In this case, the RRO value $Wr1$ and the phase $\theta r1$ may be directly calculated by numerically analyzing the measurement result of the RRO without determining the primary wave form.

In this case, the RRO value $Wr1$ corresponds to an amplitude of the primary wave form, and a center displacement δ (an eccentricity δ) of the wheel rim 1 substantially corresponds to one half of the RRO value $Wr1$. Further, the phase $\theta r1$ corresponds to a phase (an angle) in a peripheral direction of the wheel rim 1 from a predetermined reference position O (0°), and an air valve position may be appropriately set as the reference position O, for example.

Further, the weight unbalance of the wheel rim 1 can be measured by using a well-known measuring device such as an unbalance measuring device (so-called balancer), and it is possible to obtain the unbalance level Wub of the heavy point, and the phase θub (the phase from the reference position O). In this case, the unbalance level Wub means a value obtained by converting into a gravity of the balance weight mounted to a position of the distance L apart from the axis center i of the wheel rim in a radial direction (the balance weight mounting position), in other words, a gravity of the balance weight capable of balancing with the unbalance level Wub when the balance weight is mounted to the position in a side of the light point. The leading end of the rim is generally set to the balance weight mounting position.

Further, the weight unbalance of the tire 10 can be measured by the unbalance measuring device or the like in the same manner as that of the

wheel rim 1, and the phase αt of the light point (the phase from the reference position O) can be obtained.

Next, description will be given of the correction unbalance W_c obtained by correcting the weight unbalance of the wheel rim 1 by the primary component of the RRO corresponding to the substantial eccentricity δ of the wheel rim 1.

The tire 10 is approximately concentrically attached to the rim sheet 1a, as shown in Fig. 5A. On the contrary, in the rim sheet 1a, the eccentricity δ corresponding to one half of the RRO value W_{r1} is generated between a center j of the rim sheet 1a and the wheel rim axis center i (the center of rotation). Therefore, the moment corresponding to the product $T_t \times \delta$ of the tire weight T_t and the displacement δ is applied around the wheel rim axis center i . Accordingly, the further weight unbalance is generated.

Therefore, as shown in Figs. 2 and 5B, it is necessary to use a new correction unbalance vector $\overline{W_c}$ corrected by adding the weight unbalance vector $\overline{W_{ub}}$ of the wheel rim 1 itself to the weight unbalance vector $\overline{W_1}$ based on the RRO.

$$(\text{Vector } \overline{W_{ub}}) + (\text{Vector } \overline{W_1}) = (\text{Vector } \overline{W_c})$$

Herein, the vector $\overline{W_c}$ is expressed by an xy coordinate (x1, y1). As shown in Fig. 2, the xy coordinate (x1, y1) is expressed by the following equation.

$$x1 = W_{ub} \times \cos \theta_{ub} + W_1 \times \cos \theta_{r1}$$

$$y1 = W_{ub} \times \sin \theta_{ub} + W_1 \times \sin \theta_{r1}$$

Further, the value W_1 is expressed by the formula $T_t \times \delta / L$, that is, $(W_{r1} \times T_t) / (2 \times L)$ by converting into the gravity of the balance weight.

Accordingly, the phase θ_c of the vector \overrightarrow{Wc} is expressed by the following formula (1).

$$\begin{aligned}\theta_c &= \text{Tan}^{-1}(y1/x1) \\ &= \text{Tan}^{-1}[[Wub \times \text{Sin } \theta_{ub} + \{(Wr1 \times Tt)/(2 \times L)\} \times \text{Sin } \theta_{r1}]/[Wub \times \text{Cos } \theta_{ub} + \{(Wr1 \times Tt)/(2 \times L)\} \times \text{Cos } \theta_{r1}]] \dots (1)\end{aligned}$$

It is possible to enhance the effect of canceling the weight unbalance of the tire 10 to the maximum by assembling the tire and the wheel rim in a state of aligning the phase θ_c of the correction unbalance Wc obtained by substituting the respective values determined in step S1 for the formula (1), with the phase α_t of the light point of the tire 10. As a result, it is possible to reduce the gravity of the balance weight assembled for correcting the unbalance of the assembled structure of the tire and the wheel rim, after assembling.

The description has been given of the particularly preferable embodiment in accordance with the present invention. However, the present invention is not limited to the embodiment, and can be carried out by modifying into various aspects.

EXAMPLE

Two kinds of wheel rims 1A and 1B each having a rim size of 6JJ \times 15 were prepared, and there were measured the RRO value $Wr1$ in the primary component of the RRO of each of the wheel rims 1A and 1B, the phase θ_{r1} of the peak position thereof, the unbalance level Wub of the heavy point in the weight unbalance of the wheel rim, the phase θ_{ub} thereof, and the radial distance L of the balance weight sticking position for correcting the weight

unbalance from the axis center of the wheel rim. The results of measurement are shown in Table 1.

Table 1

	Wheel rim 1A	Wheel rim 1B
RRO Value W_{r1}	0.39 mm	0.45 mm
Phase θ_{r1}	40°	85°
Unbalance level W_{ub}	18 g	17 g
Phase θ_{ub}	0°	0°
Distance L	190 mm	190 mm
Phase θ_c	13.4°	30.9°

Further, nine tires each having a tire size of 195/65R15 and a tire weight T_t (9100 g) were prepared, and there were measured the weight unbalance level W_t and the position of the light point in each of the tires. The weight unbalance levels W_t were (3 g, 10 g, 12 g, 19 g, 26 g, 30 g, 33 g, 40 g, 46 g), respectively.

Further, the phase θ_c of the correction unbalance W_c in each of the wheel rims 1A and 1B was determined by using the formula (1), and the results are shown in Table 1.

Next, the wheel rims 1A and 1B, and nine tires were assembled, and the gravity of the balance weight required for correcting the unbalance of the assembled structure was compared after assembling. The results are shown in Table 2. In this case, in Comparative Example, the wheel rim and the tire are assembled in a state of aligning the phase θ_{ub} of the heavy point of the wheel rim with the phase α_t of the light point of the tire. In Example, the wheel rim and the tire are assembled in a state of aligning the phase θ_c of the correction unbalance with the phase α_t of the light point of the tire.

Table 2

Wheel rim 1A				Wheel rim 1B			
Unbalance level Wt of tire	Comparative Example	Example	Weight reduction effect	Comparative Example	Example	Weight reduction effect	
3 g	23 g	23 g	0 g	18 g	17 g	1 g	
10 g	16 g	14 g	2 g	13 g	10 g	3 g	
12 g	14 g	13 g	1 g	12 g	9 g	3 g	
19 g	8 g	5 g	3 g	11 g	3 g	8 g	
26 g	7 g	1 g	6 g	13 g	7 g	6 g	
30 g	8 g	2 g	6 g	16 g	9 g	7 g	
33 g	11 g	9 g	2 g	19 g	14 g	5 g	
40 g	17 g	14 g	3 g	25 g	19 g	6 g	
46 g	22 g	20 g	2 g	30 g	25 g	5 g	

As shown in Table 2, it can be confirmed that in Example, the effect of canceling the weight unbalance is enhanced and the gravity of the balance weight can be reduced. A relation between the weight unbalance level W_t of the tire in Table 2 and the effect of reducing the gravity of the balance weight is shown in Figs. 6A and 6B. As shown in the figures, it is confirmed that the effect of reducing the gravity of the balance weight in accordance with the present invention is more effectively achieved in a range of the weight unbalance level W_t between 15 and 45 g.

As mentioned above, in accordance with the present invention, the new correction unbalance is determined by correcting the weight unbalance of the wheel rim by the RRO primary component corresponding to the substantial eccentricity of the wheel rim, and the tire and the wheel rim are assembled in a state of aligning the phase of the correction unbalance with the phase of the light point of the tire. It is therefore possible to enhance the effect of canceling the weight unbalance to the maximum, and it is possible to further reduce the gravity of the balance weight.